Development and Characterization of Wax Molds for 3D Microfluidic Applications

Rex Garland, Jonah Kohen, Fengjiao Lyu

Mentors: David Huber, Michelle Rincon

Introduction

- 2D microfluidics can be easily realized with known lithography techniques.
- "2d+" microfluidics: stacking laminate sheets (e.g. Paul Yager, University of Washington), vias between 2d devices
- 3D microfluidics require new techniques
 - Laser-induced curing of PDMS -- 5um resolution, but requires a pulsed femtolaser (Ref: Juodkazis, 2013)
 - 3d printed molds





Ref: M Juodkazis anz, 2001.

3d Wax Printing

- Printing precise, one-time designs overnight, "rapid" prototyping
- Printing truly 3d microfluidic molds (e.g. cannot be created without the use of support material during printing)
- Microfluidic applications
 - Precision valves
 - radial sheath flow for better flow focusing

Overall Procedure:

- 1. CAD 3d model, export .stl
- 2. Run print overnight
- 3. Remove support material in print
- 4. Clean printed model

ExFab contains the **SolidScape 3ZStudio 3D Wax Printer.** This printer was originally designed for jewelers to create wax molds for casting.

Solidscape Studio Capabilities	Nominal Capabilities	Measured Capabilities	
Z-axis layer	~6 um	~14 um	
Minimum feature size	250um	200um	
Droplet size	76 um	~150um	
Surface Roughness	0.9-1.6 um	0.6-1.2 um	
X-Y positioning	197 dots/mm (~5um)		
Approximate Print Rate (including setup, auto- calibration)		5 min/mm^3 (very slow)	



Our Solution

- Use wax printer to create inverted microfluidic mold ("print the flow")
- PDMS or epoxy poured over the mold to define channel
- Melt wax out of channel after casting
- Bond channel to substrate (e.g. glass slide)





Application: Radial Sheath Flow





Characterization: Screening Test



Grid Size (um)	Approximate Line Roughness (um)	
500		30
250		37

- Agitation causes structures with aspect ratio > 2 to break
- Angle of grids has little effect on performance.

Cylinder Aspect Ratio	Survived Post- Processing?	
1	yes	
1.5	yes	
2	no	
2.5	no	



Characterization: Surface Roughness

Optical images show what appears to be surface roughness dependent on surface height (possibly due to error in vertical rastering with respect to ideal cad model) -> after testing, this theory proved wrong.



Step roughness characterization model

Surface roughness at various step heights -> no correlation



Characterization: Aspect-Ratio Test



Characterization print: various prisms

	<mark>5</mark>	11	17
	0.4, 0.8, 0.8	0.4, 0.4, 0.2	0.2, 0.4, 0.8
	<mark>6</mark>	<mark>12</mark>	<mark>18</mark>
	0.4, 0.8, 0.4	0.4, 0.4, 0.1	0.2, 0.4, 0.4
1	7	13	19
0.8, 0.8, 0.8	0.4, 0.8, 0.2	0.2, 0.8, 0.8	0.2, 0.4, 0.2
2	<mark>8</mark>	14	20
0.8, 0.8, 0.4	0.4, 0.8, 0.1	0.2, 0.8, 0.4	0.2, 0.4, 0.1
<mark>3</mark>	<mark>9</mark>	15	<mark>21</mark>
0.8, 0.8, 0.2	0.4, 0.4, 0.8	0.2, 0.8, 0.2	0.2, 0.2, 0.8
4	10	<mark>16</mark>	
0.8, 0.8, 0.1	0.4, 0.4, 0.4	0.2, 0.8, 0.1	

Structure Incides, Dimensions (I,w,h) (mm)



Optical images of top surfaces. All images same scale, vertical aspect ratios given.

Printer can handle aspect ratio of 4, as long as minimum feature is >=200um.

As in the case of grids, squares lose their structure at smaller dimensions.

The remaining (<=100um) structures did not successfully print.

Characterization: Aspect-Ratio Test 2





Structure Index	Pillar Dimensions (w, h) (mm)	Aspect Ratio	Yield
1	0.4, 1.6	4.0	100%
2	0.4, 0.8	2.0	100%
3	0.2, 0.8	4.0	68%
4	0.2, 0.4	2.0	72%
5	0.1, 0.4	4.0	0%
6	0.1, 0.2	2.0	0%

- Last two structures did not print (100um width pillars)
- ~70% yield for 200um pillars
- Difficult to remove mineral oil from within pillars



Characterization: Well Test



Structure Index	CAD width (mm)	CAD depth (mm)	Actual depth (mm), %depth
1	0.4	0.2	0.2 (100%)
2	0.4	0.4	0.4 (100%)
3	0.4	0.8	0.8 (100%)
4	0.2	0.2	0.2 (100%)
5	0.2	0.4	0.4 (100%)
6	0.2	0.8	0.4 (50%)
7	0.1	0.2	0.2 (100%)
8	0.1	0.4	0.4 (100%)
9	0.1	0.8	0.25 (31%)
10	0.05	0.2	DID NOT PRINT
11	0.05	0.4	0.24 (60%)
12	0.05	0.8	0.2 (25%)



- All support wax dissolved after light ultrasound, but >4 aspect ratio failed
- Large pitting (~50um diameter) occurred in build material after ultrasound.



pitting

Procedure

- Desired STL files are loaded into 3ZWorks and the .3zs file is generated.
- .3zs file is loaded via USB Drive to the printer. Job starts.
- Once job completes, molds need to be scraped off of the build plate.
- Red support material removed via a mineral oil bath



Challenges: Channel Thickness

- Although the printer advertises 6 um resolution, it was impossible to manufacture channels below 100 um in thickness.
- Previous characterizations of the wax printer did not print features below 250 um thickness.
- The 6 um resolution most likely is responsible for the smooth edges seen on round features.







Challenges: Warping

- Caused by uneven temperature gradients when the molds are being submerged in the heated bath.
- Once warping occurs, it is irreversible, and the mold is rendered useless.
- Solutions:
 - Be sure not to leave molds in the bath no longer than an 1.5 hours.
 - Place molds on an elevated surface so that they do not touch the glass bottom.





Challenges: Residue

- There are three main residues we encountered during this project that proved troublesome: brown thermal residue, blue build residue, leftover support material.
- Thermal residue results if molds are left too long in too cold a bath.
- Build residue results if vacuum bag on printer isn't replaced enough.
- Support material may take longer to remove in larger molds. Second dip is necessary.







Mold Cleanliness: Two Outcomes



- BAD: Darker blue on surface - mineral oil absorbed by build material power generated during print
- Appears grainy under microscope
- ~20um roughness

- **GOOD**: Lighter blue no powder
- Streaks under microscope show printer rastering
- ~4um roughness (more cleaning needed to get 1 um)











Results: Successful Molds!





I have a well paying job!

- Molds without warping, residue, or broken features were generated.
- A step-by-step guide for generating perfect molds has been created and will be added to the lab wiki.
- These molds may now be used to generate microfluidic structures.



Fabrication of microfluidic channels

Materials	Description	Vendor	Uncured mixed viscosity (cps)	Tensile strength (MPa)	Young's modulus	Working time	Curing time and condition	Color
PDMS	Polydimethyl siloxane, prototyping polymer	Dow Corning	5550	2.2	360-870 kPa	NA	~2 hrs (@65°C)	Clear
Conapoxy FR-1080	High temperature epoxy	Cytec Industries	2500	29	2.7 GPa	>2 hrs	4-16 hrs (@120°C)	
5-Minute Epoxy	Rapid-curing	Devcon	10000	13	1.2 GPa	3-6 mins	0.75-1 hrs	Light
2-Ton Epoxy	Героху	Devcon	8000	16	1.5 GPa	30-35 mins	~2 hrs	amber
SU-8 3005			70					
SU-8 2025	Epoxy-based		5485				radiation (avpacure	
SU-8 2075	negative	MicroChem	27192	60-75	2.0 GPa	NA	laulation (exposule	
SU-8 5	U-8 5 photoresist		338				thicknoss)	
SU-8 100			60000					

Fabrication of microfluidic channels

Material	Pros	Cons	Comments
PDMS	Soft Clear Easy to bond Thermostability	Too flexible for some 3D structures	Widely used for the fabrication and prototyping of microfluidic chips
Rapid- curing epoxy	Strong 3D structure Short curing time	Hard Fragile Bubble Wax removal problem Distorted when heating to 100°C Hard to bond	Adding organic solvent, such as ethanol, can decrease stiffness and increase curing time for bubble removal. But most organic solvents can dissolve wax mold.
SU-8	Strong 3D structure Photocuable (radiation curing) Thermostability	Expensive (relatively) Bubble Hard to bond	There are a series of SU-8 with some different performances. But as a epoxy-based material, SU-8 has a lot of similar properties with normal epoxy.



PDMS channel



Epoxy channel

• Experimental Setup

- Inner flow: 0.05-0.2 mL/hr, 200-400 μm
- Sheath flow: 1-2 mL/hr, 1-2 mm
- Calculation and estimation
 - Reynolds number
 - Maximum Re $\approx 0.8 << 2000$
 - Laminar flow
 - Péclet number
 - $Pe \approx 64000$
 - Fluid remains largely unmixed

$$\operatorname{Re} = \frac{\rho v L}{\mu}$$

$$\mathrm{Pe} = rac{\mathrm{advective\ transport\ rate}}{\mathrm{diffusive\ transport\ rate}}$$
 $\mathrm{Pe}_L = rac{Lu}{D} = \mathrm{Re}_L \ \mathrm{Sc}$

- Result
 - Laminar flow
 - Sheath flow in vertical direction







- Problem
 - No radial sheath flow
 - Big diameter of sheath flow channel
 - Flexible inner flow channel (suspended)







	Traditional microfluidic channel fabrication		Our method using 3D wax printer
•	Time-consuming (~1 week) 2D (stacking for "2D+")	•	Rapid (~1 day) 3D
•	High resolution (~5 µm)	•	Low resolution (~200 µm)

- Conclusion
 - Wax printer is a great tool for rapid prototype at large scale.
 - 3D microfluidic device can be fabricated using wax printer.
- Future plan
 - Add more symmetric support for the suspended channel
 - Decrease the diameter and flow rate of the sheath flow
 - Iterations for channel design

Thank you! Q&A

• Reference

- Hofmann, Oliver, Philippe Niedermann, and Andreas Manz. "Modular Approach to Fabrication of Three-Dimensional Microchannel Systems in PDMS application to Sheath Flow Microchips." Lab Chip 1, no. 2 (2001): 108–14. doi:10.1039/B105110P.
- Rekštytė, Sima, Mangirdas Malinauskas, and Saulius Juodkazis. "Three-Dimensional Laser Micro-Sculpturing of Silicone: Towards Bio-Compatible Scaffolds." Optics Express 21, no. 14 (July 15, 2013): 17028. doi:10.1364/OE.21.017028.